Submitted to:

City of Winnipeg

SLOPE STABILITY ASSESSMENT AND PROPOSED STABILITY IMPROVEMENTS LOT 16 DRAIN, WINNIPEG, MANITOBA



FEBRUARY 2024

FILE NO. 20-217-01



"Engineering and Testing Solutions That Work for You"

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City of Winnipeg Slope Stability Assessment and Proposed Stability Improvements Lot 16 Drain, Winnipeg, Manitoba File No. 20-217-01



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ATTACHMENTS

- Figure 1 Existing Site, Test Hole Location Plan and Photographs 1 and 2
 Figure 2 Overall Site Plan, Test Hole Location Plan, and Cross Section Overlay
 Figure 3 Overall Site Plan and Test Hole Location Plan
 Figure 4 Slope Stability Analysis Result on Cross Section 1, 2 and 3

- Figure 5 Slope Stability Analysis Result on Cross Section 4 and 5
- Figure 6 Photographs 3-8
- Soil Classification Sheet
- Test Hole Summary Logs (9)



1.0 INTRODUCTION

ENG-TECH Consulting Limited (ENG-TECH) completed the requested slope stability assessment for a channel bank known as Lot 16 Drain located between Brady Road and Bishop Grandin Boulevard in Winnipeg, Manitoba. ENG-TECH understands that the channel bank movements have occurred within +/- 1300 m of the North end of the channel. The purpose of the assessment is to evaluate the overall stability and provide remedial options to stabilize this section of the channel bank.

1.1 Scope of Work

ENG-TECH completed the following scope of work:

- Survey of the channel bank in the zones of concern including several cross sections and spot elevations.
- A test hole drilling and soil sampling program.
- Review of the existing information about the site and nearby properties.
- Installation and monitoring of a groundwater vibrating wire piezometer (VW) to evaluate the groundwater condition.
- A slope stability assessment of the channel bank and report outlining the geotechnical investigation and recommendations as outlined in the introduction.

2.0 BACKGROUND

ENG-TECH supervised the drilling of nine (9) test holes (TH1-TH9) at Lot 16 Drain, Winnipeg, Manitoba, on April 13, 2020.

The test holes were drilled using a CME-55 Track-Mounted drill rig equipped with 125 mm diameter solid stem continuous flight augers owned and operated by Maple Leaf Drilling Ltd. TH6 and TH8 were advanced to 7.6 meters below grade (mbg), while TH1-TH5, TH7 and TH9 were drilled to 3.0 mbg. Soil samples were collected off auger flights at select depth intervals. The soil stratigraphy was visually classified using the modified Unified Soil Classification System (USCS) during drilling. Pocket Penetrometer field tests were completed at various depth intervals during drilling to evaluate the consistency of the cohesive soils with depth. One (1) Vibrating Wire Piezometer was installed in TH8 at depths of 7.0 m mbg.

In ENG-TECH's Winnipeg laboratory, moisture contents were completed on all soil samples collected (46) and three (3) Atterberg Limit tests, three (3) hydrometer tests, and four (4) unconfined tests were completed on selected samples. All laboratory test results are shown on the test hole summary logs, with the particle size results shown on a separate graph.





3.0 STRATIGRAPHY

Based on the results of the drilling program, the following summarizes the general soil stratigraphy at the subject property:

- The stratigraphy consisted of clay followed by silt in TH1. The stratigraphy in TH2 consisted of clay fill, followed by clay, and then silt. In TH3 and TH9, the stratigraphy consisted of clay fill followed by clay. The stratigraphy consisted of clay fill, followed by a layer of clay, followed by a silt layer overlaying high plastic clay in TH4-TH8.
- The clay fill was mostly medium brown to medium grey, frozen, highly plastic, and contained some to with silt and trace sand. Salts were observed in TH3 and TH4.
- The clay was mostly medium brown to dark grey, highly plastic, firm to very stiff (frozen until 1.5- 2.0 m), trace sand, some silt, oxidation in TH4 and salts in TH5 and TH6.
- The silt layer was light brown to light grey, wet, soft, low plastic, trace gravel in TH1, trace sand in TH1 & TH7, some sand in TH2, TH4, TH5, TH6, and TH8, and some clay in TH1-TH2, and TH4-TH8.

Detailed stratigraphy descriptions are outlined on the attached test hole summary logs.

4.0 TOPOGRAPHIC SURVEY AND SITE VISITS

A survey of the property consisting of spot elevations and twelve (12) cross-sections was completed by ENG-TECH personnel using GPS and total station survey equipment on April 16 and April 24, 2020 and August 24, 2022. Additionally, lidar data was provided by the City of Winnipeg for referencing the existing drainage system.

The topography at the site is relatively flat from the existing field to an existing swale on the south bank of the channel and then slopes up to the top of the south channel bank, where it starts sloping down towards the channel with a slope of approx. 5.5H:1V. There was evidence of local and global slope failures throughout the entire south channel bank.

The piezometer was installed in TH8 at a depth of 7.0 mbg in the high plastic clay layer. Table 1 shown on Figure 1 outlines the results of the readings of the VW piezometer. As shown in Table 1, the groundwater (GW) fluctuated between 229.78 m and 229.89 m during the monitoring period between April 2020 and November 2020. A conservative GW value of 233.0 m was used in all the slope stability analyses to model an extreme GW condition.

5.0 SLOPE STABILITY ASSESSMENT

5.1 General

Slope stability analysis was completed using SLOPE/W, a two-dimensional finite element analysis computer program. The analysis was completed to assess the channel stability considering its existing condition. The soil and geometry conditions used in the analysis are shown on Figure 4.





5.2 Assessment Criteria

- The soil shear strength parameter values used should be representative of the in-situ soils;
- The GWL should be representative of GW conditions at the site.
- The combined GW and channel water level used in the analysis should be representative of a conservative condition that is normally not experienced at the property.

5.3 Soil and Groundwater Values

The assessment was conducted based on both post-peak and residual values for clay shear strength properties. The results of both analyses were recorded and compared in order to examine the effect of the brown clay shear strength properties on the overall slope stability of the riverbank. Visual inspection showed evidence of slope failure on the southern channel bank in the clay fill layer, therefore, residual shear strength values were used for the clay fill in all the analyses. Outlined below are the soil shear strength values and water levels used in the model.

Stiff Brown Clay (CH)	Unit Wt = 18 kN/m^3	c′ = 2 kPa	φ' = 15°		
Silt	Unit Wt = 18 kN/m^3	c' = 0 kPa	φ' = 19°		
Clay Fill	Unit Wt = 18 kN/m^3	c' = 0 kPa	φ' = 12°		
Residual Soil	Unit Wt = 18 kN/m^3	c' = 1 kPa	φ' = 12°		
Extreme GWL	Elev. = 233.0 m				
Channel Water Level	Elev. = 2	231.0 m			

The above assumptions do not necessarily represent a combined GW and channel water level condition that has been experienced at the property. However, they are considered a worst-case GW and channel water level condition.

5.4 Methodology

ENG-TECH evaluated five (5) cross-sectional profiles based on the soil and topographic characteristics. The location of the cross-sections and the sectional profiles are shown on Figure 1-5. The stability assessment of the slope was completed using Morgenstern-Price circular slip surfaces with a half-sine interslice force function to estimate the FS of potential slip surfaces (PSSs). Various PSSs were assessed to evaluate the FSs against slope failure.

5.5 Results and Assessment

Based on the results of the analysis, the channel bank requires stabilization measures. ENG-TECH examined different stabilization measures and provided the City of Winnipeg with different channel bank stabilization options, such as using sand drains, offloading with multiple slopes and also offloading with a single slope. Based on the preliminary estimated quotes ENG-TECH received for each option from contractors, and consulting with the City of Winnipeg, offloading with a single slope was chosen as the stabilization measure. Below is a summary of the proposed work with detailed illustrations shown on Figures 4 and 5.



City of Winnipeg Slope Stability Assessment and Proposed Stability Improvements Lot 16 Drain, Winnipeg, Manitoba File No. 20-217-01



Slope Stabilization

The City of Winnipeg expressed interest in stabilizing the area of the channel bank from Kenaston Boulevard to Eldorado Boulevard, which is approx. 1300 m long, by offloading and building a new berm on the south bank. This section consists of a 75 m curved section, up to STA 0+075, and a 1225 m straight section to the end at STA 1+300. The results of the slope stability analysis show that offloading the bank with a single slope of 7H:1V provides adequate stability for the channel bank and produces FSs acceptable for slope stability (Figures 4 and 5). Overall, the FSs of all PSSs will improve significantly after the offloading and placing fill for the new berm. The most critical PSSs of each cross-section are detailed in the table below:

Cross		Post-peak	Assessment	Residual Assessment		
section	Most critical PSS	Existing Condition	With Offload and Backfill	Existing Condition	With Offload and Backfill	
1	PSS2 (Figure 4)	1.20	1.39	1.11	1.30	
2	PSS3 (Figure 4)	1.13	1.83	0.99	1.64	
3	PSS2 (Figure 4)	1.26	1.62	1.12	1.42	
4	PSS3 (Figure 5)	1.18	1.96	0.99	1.66	
5	PSS3 (Figure 5)	1.13	>2	0.83	1.54	

As shown in the table above, all the FSs increased to more than 1.30 in both post-peak and residual assessments, and are acceptable for slope stability. The above stabilization work will result in 16,200 m³ of soil offloaded from the bank and 5650 m³ of backfill placed for the construction of the new berm, as shown on Figures 4 and 5.

Channel Erosion Protection

Some erosion was observed in the channel bank during the site visits. Installing erosion protection can help reduce the amount of erosion and can also slightly further improve the channel bank's stability. Placing a 0.3 m thick layer of rip-rap stone on the south bank will provide adequate erosion protection for the bank. Placing erosion protection is optional at this time and can be completed after the channel bank's stabilization work.

New Berm

The top of the new berm elevation was mandated by the City of Winnipeg to be at 234.0 m to prevent channel overflow. The side slope of the new berm on the channel side, as shown on Figures 4 and 5, matches with the 7H:1V offload of the existing bank, while the field side slope of the berm is designed at 3H:1V. From STA 0+000 to STA 0+350, the width of the berm top is 0.6 m and this width gradually increases to 3.0 m from STA 0+350 to STA 0+400, after which the width remains constant at 3.0 m. The dimensions and location of the new berm are shown on Figures 2, 3, 4 and 5.

New Swale

The existing swale had to be filled and removed due to the construction of the new berm. As mandated by the City of Winnipeg, a new swale should be constructed at the location shown on Figures 2 and 3. The new swale should be constructed closer to the field and further from the channel due to the location of the new berm.





The location and all the elevations of the new swale were chosen under the City of Winnipeg's direction and solely based on the location of the new berm. The drainage and flow capacity, water flow directions and all other hydraulic and drainage-related properties of the new swale must be checked, verified and modified (if necessary) before the commencement of any field construction.

6.0 STATEMENT OF LIMITATIONS AND THIRD-PARTY USE

The geotechnical information provided in this report is in accordance with acceptable engineering principles and practices (Standard of Practice). The findings of this report were based on information provided (field investigation and laboratory testing). Soil conditions are natural deposits that can be highly variable across a site. If sub-surface conditions are different than the conditions previously encountered on-site or those presented here, we should be notified to adjust our findings if necessary.

All information provided in this report is subject to ENG-TECH's standard terms and conditions for engineering services, a copy of which is provided to each of our clients with the original scope of work, or a mutually executed standard engineering services agreement. If these conditions are not attached, and you are not already in possession of such terms and conditions, contact our office and you will be promptly provided with a copy.

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7.0 CLOSURE

This report was based on the scope of work outlined for the purpose of the investigation and was prepared in accordance with acceptable professional engineering principles and practices. If you have any questions, please contact the undersigned.

Sincerely,

ENG-TECH Consulting Limited

Arash Gholamzadehabolfaz, M.Sc., E.I.T. Engineering Department

CDH/ag



Clark Hryhoruk, M.Sc., P. Eng. Principal, Geotechnical Engineer





MAJOR DI	VISION				
		GROUP SYMBOL	GRAPH SYMBOL	TYPICAL DESCRIPTION	LABORATORY CLASSIFICATION CRITERIA
뿌ᇦᄩ	CLEAN GRAVELS (TRACE OR NO	GW		WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES	$C_U = \frac{D_{60}}{D_{10}} > 4$; $C_C = \frac{(D_{30})^2}{D_{10} \times D_{60}} = 1 \text{ TO } 3$
R THAN 75 µm) GRAVELS THAN HALF TH RSE FRACTION R THAN 4.75 m	FINES)	GP	2000	POORLY GRADED GRAVELS, GRAVEL- SAND MIXTURES, LITTLE OR NO FINES	NOT MEETING ABOVE REQUIREMENTS
GRAVELS GRAVELS GOARSE FRACTION LARGER THAN 4.75 mm	DIRTY GRAVELS (WITH SOME OR	GM	9000	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES	ATTERBERG LIMITS BELOW "A" LINE OR P.I. LESS THAN 4
BY WEIGHT LARGER THAN 75 µm) GRAVELS MORE THAN HALF TH COARSE FRACTION LARGER THAN 4.75 nm)	MORE FINES)	GC	9000	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES	ATTERBERG LIMITS ABOVE "A" LINE AND P.I. MORE THAN 7
	CLEAN SANDS (TRACE OR NO	sw		WELL GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES	$C_U = \frac{D_{60}}{D_{10}} > 6$; $C_C = \frac{(D_{30})^2}{D_{10} \times D_{60}} = 1 \text{ TO } 3$
(MORE THAN HALF SANDS MORE THAN HALF THE COARSE FRACTION SMALLER THAN 4.75 mm	`FINES)	SP		POORLY GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES	NOT MEETING ABOVE REQUIREMENTS
SAI ORE THA COARSE	DIRTY SANDS (WITH SOME OR	SM		SILTY SANDS, SAND-SILT MIXTURES	ATTERBERG LIMITS BELOW "A" LINE OR P.I. LESS THAN 4
	MORE FINES)	SC		CLAYEY SANDS, SAND-CLAY MIXTURES	ATTERBERG LIMITS ABOVE "A" LINE AND P.I. MORE THAN 7
SILTS BELOW "A" LINE NEGLIGIBLE ORGANIC CONTENT	LL ≤ 50%	ML		INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY SANDS OF SLIGHTY PLASTICITY	
SI BELOW NEGL ORC	LL > 50%	МН		INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS, FINE SANDY OR SILTY SOILS	
SWALLER :	LL ≤ 30%	CL		INORGANIC CLAYS OF LOW PLASTICITY, GRAVELLY, SANDY OR SILTY CLAYS, LEAN CLAYS	
LE BY WEIGHT SMALLE CLAYS ABOVE "A" LINE NEGLIGIBLE ORGANIC CONTENT	30% < LL ≤ 50%	CI		INORGANIC CLAYS OF MEDIUM PLASTICITY, SILTY CLAYS	CLASSIFICATION IS BASED UPON PLASTICITY CHART
HALF BY	LL > 50%	СН		INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS	(SEE BELOW)
(MORE THAN HALF BY WEIGHT SMALLER THAN 75 µm) ORGANIC SILTS & CLAYS & CLAYS & CLAYS BELOW "A" LINE ORGANIC CONTENT CONTENT CONTENT CONTENT CONTENT CONTENT CONTENT CONTENT	LL < 50%	OL	1//	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	
(MO) ORGAN & CL BELOW	LL > 50%	ОН		ORGANIC CLAYS OF HIGH PLASTICITY	
HIGHLY INORG	SANIC SOILS	Pt	***** *****	PEAT AND OTHER HIGHLY ORGANIC SOILS	STRONG COLOUR OR ODOUR, AND OFTEN FIBROUS TEXTURE

TILL		SANDSTONE	
TILL		GRANITE	++++++++
FILL			
TOPSOIL	2222		
CONCRETE	1 : 4		
SHALE			
LIMESTONE			

60	LOW -	INTERMEDIAT	E HIG	4.1	
50	LOW	(MEDIUM)	nic	in	
í			СН	/	
50 — 40 — 30 —			3/2		
		CI	"A"LIME		
30				он & мн	
20	CL			OTT G IVIIT	
20					
10	7	ML & OL			-
	4 CL-ML	ML & OL			
٥٥	10 20	30 40	50 60 7	70 80	90 10
		LIQUID L	IMIT (%)		

INTRUSIONS ROOTLETS OXIDES	CONSISTENCY VERY SOFT SOFT	PEN (TSF)	<u>(N)</u> < 2
		0.05	
IM OXIDES	SOFT	0 0 5	
		0 - 0.5	2 - 4
MICA	FIRM	0.5 - 1.0	4 - 8
GYPSUM	STIFF	1.0 - 2.0	8 - 15
ETC.	VERY STIFF	2.0 - 4.0	15 - 30
	HARD	> 4.0	> 30
	GYPSUM	GYPSUM STIFF ETC. VERY STIFF	GYPSUM STIFF 1.0 - 2.0 ETC. VERY STIFF 2.0 - 4.0

TSF x 95.8 = $kPa(q_U)$ $S_U = \frac{1}{2} \times q_U$

SOIL DESCRIPTIONS

	0 - 10%	BOULDERS:	> 200 mm	COARSE SAND:	
SOME:	10 - 20%	COBBLES:	75 - 200 mm	MEDIUM SAND:	0.425 - 2 mm
WITH:	20 - 35%	COURSE GRAVEL:	19 - 75 mm	FINE SAND:	0.075 - 0.425 mm
AND:	35 - 50%	FINE GRAVEL	4.75 - 75 mm	FINES:	< 0.075 mm
	G	RANULAR SOILS			

MOISTURE	DENSITY	GRADATION	INTRUSIONS	SPT (N)
DRY	VERY LOOSE	POORLY	ROOTLETS	0 - 4
DAMP	LOOSE	WELL	OXIDES	4 - 10
MOIST	MED. DENSE		MICA	10 - 30
WET	DENSE		FINES	30 - 50
	VERY DENSE		ETC.	> 50

DEFINITIONS LL = LIQUID LIMIT C_C = COMPRESSION INDEX PL = PLASTIC LIMIT

P.I. = PLASTICITY INDEX

C_U = COEFFICIENT OF UNIFORMITY

q_U = UNCONFINED COMPRESSIVE STRENGTH S_U = UNDRAINED SHEAR STRENGTH

1	
	ENG-TECH
	CONSULTING LIMITED

#6 - 854 Marion Street Winnipeg, MB R2J 0K4 Phone: (204) 233-1694 Fax: (204) 235-1579



Test Hole #: TH1

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

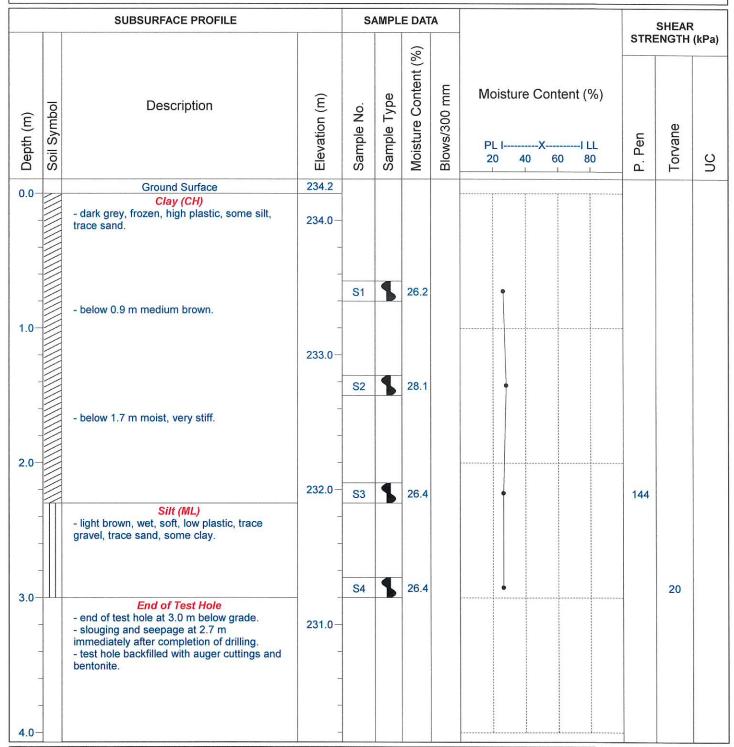
Project: Slope Stabilization Work

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.2 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

SAMPLE TYPE

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

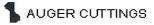
Auger Size: 125 mm

Completion Depth: 3.0 m Completion Elevation: 231.2 m

Sheet: 1 of 1

SPLIT BARREL







Test Hole #: TH2

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

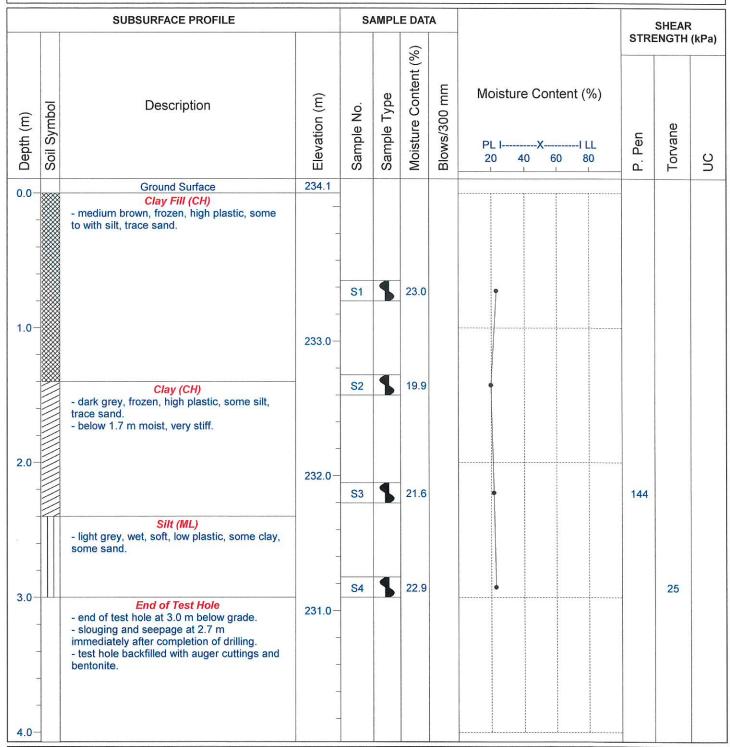
Location: See Figure 1

Solutions That Work For You **Project:** Slope Stabilization Works File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.1 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

SAMPLE TYPE

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 3.0 m Completion Elevation: 231.1 m

Sheet: 1 of 1

SPUT BARREL







Test Hole #: TH3

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.0 m

Water Elevation: --

		SUBSURFACE PROFILE		s	AMPL	E DAT	A		SHEA	R STRE	NGTH
Depth (m)	Soil Symbol	Description	Elevation (m)	Sample No.	Sample Type	Moisture Content (%)	Blows/300 mm	Moisture Content (%) PL I	P. Pen	Torvane	nc
0.0-		Ground Surface	234.0								
-		Clay Fill (CH) - medium brown, frozen, high plastic, some to with silt, trace sand, salts.	-	S1	•	24.5					
-			-	31		24.5					
1.0-		Clay (CH) - dark grey, frozen, high plastic, some silt, trace sand.	233.0						-		
_		- below 1.4 m medium brown, salts.	_	S2	\$	23.0					
2.0-		- below 2.0 m moist, very stiff.	232.0-	S3	\$	27.5		•	168		
3.0-			231.0	S4	\$	40.7		•	120		
-		End of Test Hole - end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of drilling test hole backfilled with auger cuttings and bentonite.	-								
4.0-			230.0-								

ENG-TECH Consulting Limited

Logged by: WGH

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 3.0 m

Completion Elevation: 231.0 m

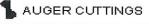
Sheet: 1 of 1

SAMPLE TYPE

Reviewed by:

SPLIT BARREL





SPLIT SPOON



Test Hole #: TH4

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 233.9 m

Water Elevation: --

Description (E) You and End of Test Hole - end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of driling est hole actifiled with auger cuttings and bentontie.		SUBSURFACE PROFILE		SA	AMPL	E DAT	Ά			SHEAR	
The strict of test Hole In a complete series of test Hole In a complete series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In a complete series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In the series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In the series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In the series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In the series of test hole at 3.0 m below grade. In sologing or seepage observed immediately after completion of drilling. In the series of test hole at 3.0 m below grade. In the se	Depth (m)	Description	Elevation (m)	Sample No.	Sample Type	Moisture Content (%)	Blows/300 mm	PL II LL	Pen	Torvane HTD	(kPa)
- medium brown, frozen, high plastic, some to with silt, trace sand, salts. S1 24.9 -1.0-	0.0		0.0								
Clay (CH) - dark grey, frozen, high plastic, some silt, trace sand below 1.4 m medium brown. Silt (ML) - light brown, moist to wet, soft, low plastic, some sand, some clay. Clay (CH) - medium brown, moist, very stiff, high plastic, some silt, trace sand, oxidation. Salt (ML) - 2.0 S3 21.6 S3 41.3 144 - end of Test Hole - end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of drilling test hole backfilled with auger cuttings and	-	 medium brown, frozen, high plastic, some 	-	S1	\$	24.9					
2.0 - light brown, moist to wet, soft, low plastic, some sand, some clay. Clay (CH) - medium brown, moist, very stiff, high plastic, some silt, trace sand, oxidation. 21.6 End of Test Hole - end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of drilling test hole backfilled with auger cuttings and		- dark grey, frozen, high plastic, some silt, trace sand. - below 1.4 m medium brown.		S2	\$	22.5		•			
- medium brown, moist, very stiff, high plastic, some silt, trace sand, oxidation. S4 41.3 End of Test Hole - end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of drilling test hole backfilled with auger cuttings and	2.0	light brown, moist to wet, soft, low plastic, some sand, some clay.	-2.0	S3	\$	21.6				25	
- end of test hole at 3.0 m below grade no slouging or seepage observed immediately after completion of drilling test hole backfilled with auger cuttings and		- medium brown, moist, very stiff, high	-	S4	1	41.3			144		
	-	 end of test hole at 3.0 m below grade. no slouging or seepage observed immediately after completion of drilling. test hole backfilled with auger cuttings and 	-3.0-								

ENG-TECH Consulting Limited

Logged by: WGH

Drilled By: Maple Leaf Drilling Ltd.
Drill Rig: CME-55 Track Rig
Auger Size: 125 mm

Completion Depth: 3.0 m Completion Elevation: 230.9 m

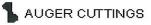
Sheet: 1 of 1

SAMPLE TYPE

Reviewed by:

SPUT BARREL









Test Hole #: TH5

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

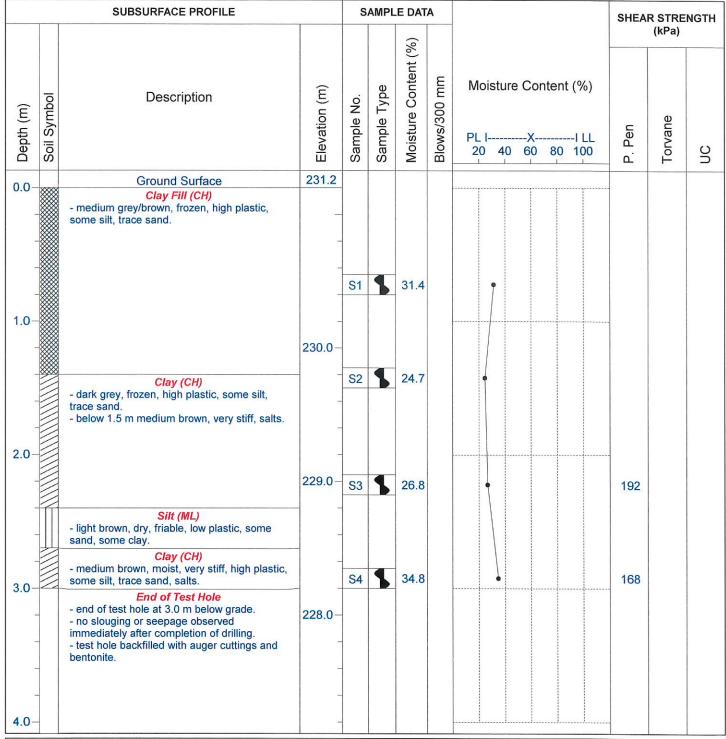
Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.2 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 3.0 m Completion Elevation: 231.2 m

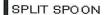
Sheet: 1 of 1

SAMPLE TYPE

SPUT BARREL









Test Hole #: TH6

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

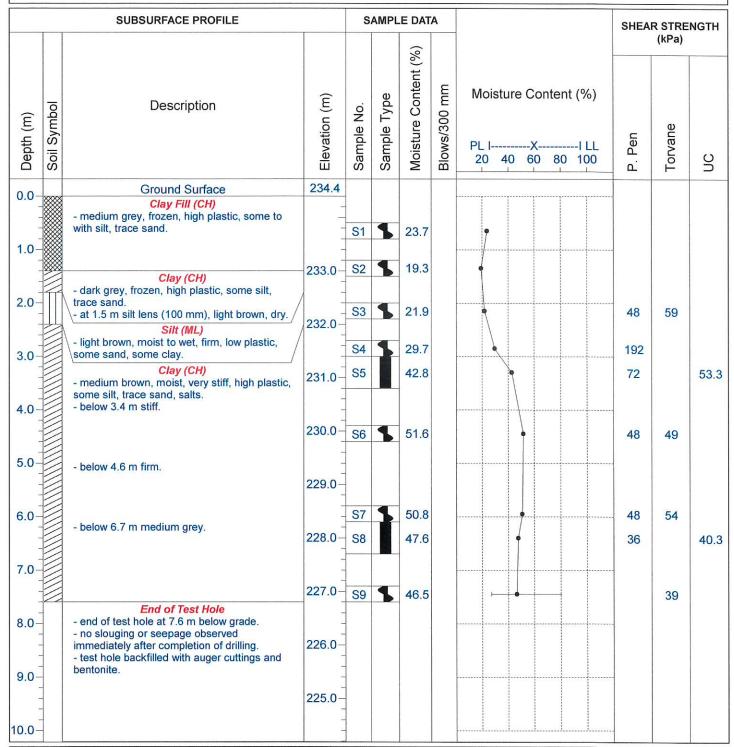
Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.4 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 7.6 m

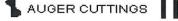
Completion Elevation: 226.8 m

Sheet: 1 of 1

SAMPLE TYPE

SPLIT BARREL









Test Hole #: TH7

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

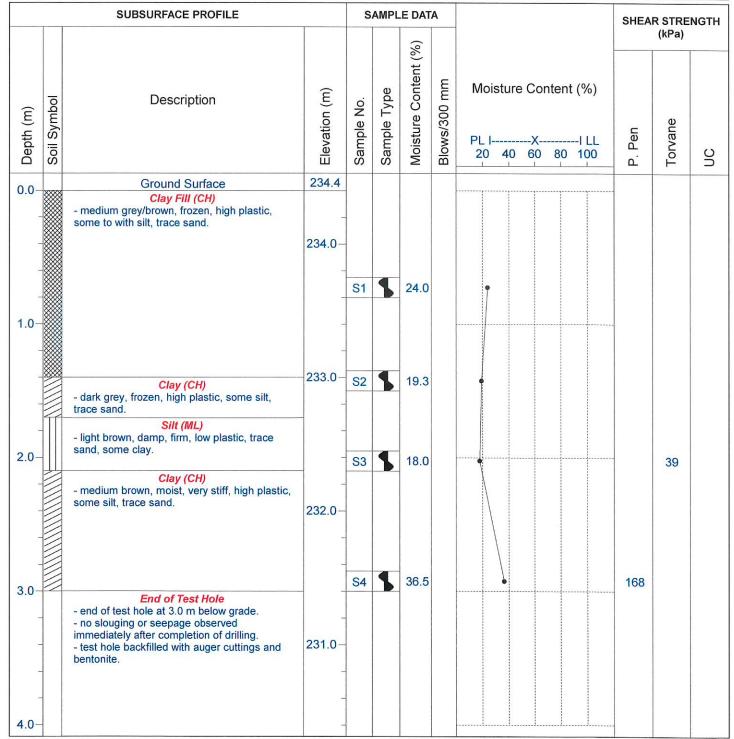
Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 234.4 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 3.0 m
Completion Elevation: 231.4 m

Sheet: 1 of 1

SAMPLE TYPE

SPLIT BARREL

SHELBY TUBE



SPLIT SPOON



Test Hole #: TH8

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

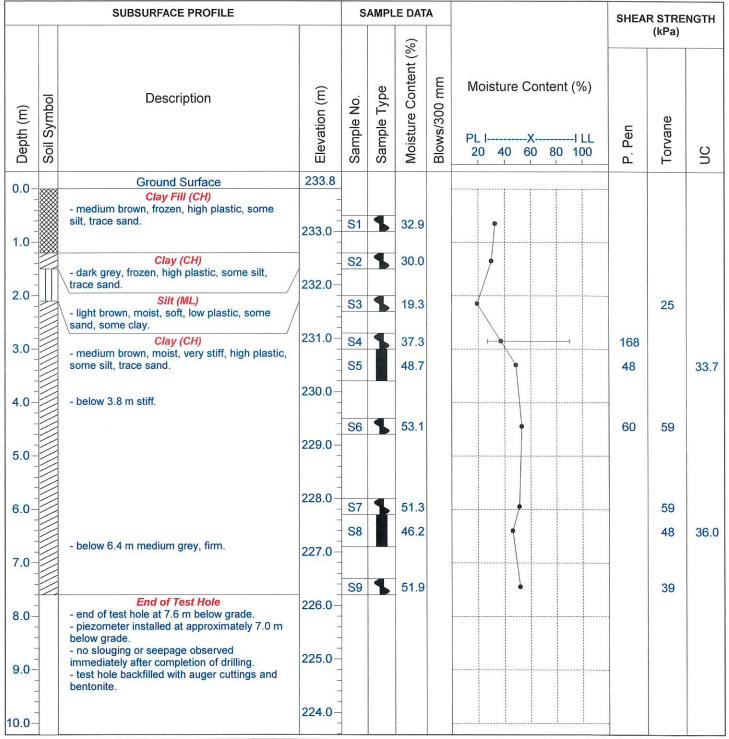
Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 233.8 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Reviewed by:

Drilled By: Maple Leaf Drilling Ltd.

Drill Rig: CME-55 Track Rig

Auger Size: 125 mm

Completion Depth: 7.6 m

Completion Elevation: 226.2 m

Sheet: 1 of 1

SAMPLE TYPE

SPUT BARREL





AUGER CUTTINGS SPLIT SPOON



Test Hole #: TH9

Client: City of Winnipeg

Site: Lot 16 Drain, Winnipeg, Manitoba

Location: See Figure 1

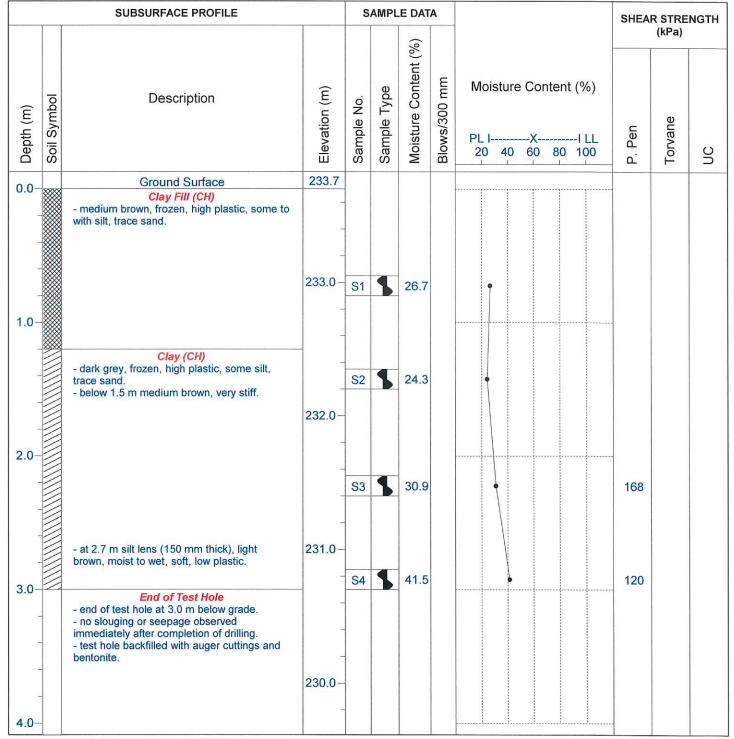
Project: Slope Stabilization Works

File No.: 20-217-01

Date Drilled: April 13, 2020

Grade Elevation: 233.7 m

Water Elevation: --



ENG-TECH Consulting Limited

Logged by: WGH

Drill Rig: CME-55 Track Rig Auger Size: 125 mm

Drilled By: Maple Leaf Drilling Ltd.

Completion Depth: 3.0 m Completion Elevation: 230.7 m

Sheet: 1 of 1

SAMPLE TYPE

Reviewed by:

SPLIT BARREL





